# Back-contacted high-efficiency silicon solar cells – conversion efficiency dependence on cell thickness

#### Cell Processing

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#### ABSTRACT

Reducing the cost of photovoltaic energy is the main objective of solar cell manufacturers. This is ideally realized by increasing cell efficiency and simultaneously decreasing manufacturing cost. To reduce fabrication costs, the international roadmap of photovoltaics (ITRPV) forecasts a reduction in cell thickness from 180µm to 120µm in the next six years, and even thinner cells may be desirable, as long as efficiency and yield are not negatively affected. In order to increase efficiency, the ITRPV forecasts an increase in share of back-contacted cells from 5% to 35% in the next eight years. In this paper the dependence of the efficiency of back-junction back-contact (BJBC) solar cells on cell thickness is investigated experimentally and numerically. To this end, BJBC silicon solar cells with cell thicknesses ranging from 45µm to 290µm are fabricated and simulated. Thinned float-zone material is used as well as monocrystalline epitaxial layers fabricated by the porous silicon process for 45µm-thick cells. The efficiency of the best cell is 22.6% (130µm cell thickness) and 18.9% for an epitaxial cell (45µm thickness). Loss mechanisms in the maximum power point of all cells are investigated by using a free-energy loss analysis based on finite-element simulations. A lower generation and a lower recombination in thinner cells compete against each other, resulting in a maximum efficiency of 20% for a cell thickness beyond 290µm, but reducing the cell thickness from 290µm to about 90µm results in a power loss of less than 0.6% absolute.

#### Introduction

Back-junction back-contact (BJBC) silicon solar cells combine a high conversion efficiency potential with a single-side cell interconnection within the module [1,2]. The advantages of the single-side cell interconnection are the reduction of handling steps [3] and the avoidance of micro-cracks by using a conductive foil [4]. By using high-throughput processes, such as ion implantation [5,6] and laser processing [7], the back-junction process may in the future reduce fabrication costs compared to the standard screen-printed solar cell process. Furthermore, the decrease in material consumption also leads to a reduction in costs.

The effect of cell thickness on solar cell efficiency has already been studied for solar cells with two-sided contacts. In 1982 Chih-Tang et al. [8], using low base lifetime material, determined a broad efficiency peak of 17% at around 50µm cell thickness. Kray et al. [9] found that efficiency is practically independent of cell thickness for Czochralski-grown material, and efficiency only slightly increases by up to 1% absolute with increasing cell thickness from 36µm to 250µm for floatzone material. In the latter study, silicon wafers with an initial thickness of 250µm were thinned down by an infeed grinder to achieve the desired thickness. However, for production this technique is obviously not feasible.

"The highest solar cell conversion efficiency achieved using the latest kerf-less technologies is only 15%, whereas a 19.1% conversion efficiency has been obtained by applying the PSI process." For this investigation, the porous silicon process (PSI) [10,11], which was first discovered in 1997, is used to fabricate  $45\mu$ m-thick crystalline silicon films. This technology skips the wafering process, in which 55% of the material is wasted (at a current wafer thickness of 180µm). Alternatives to this technique include the separation of a thin silicon film from a monocrystalline substrate wafer by annealing a stack of metal deposited on top of a silicon wafer and by using ion implantation [12,13].



Figure 1. Schematic of the porous silicon process: (a) a porous double layer is electrochemically etched in a substrate wafer – the bottom layer has a high porosity, whereas the upper layer has a low porosity; (b) the porous double layer reorganizes during a sintering step in hydrogen at 1100°C; (c) an epitaxial Si layer grows in a chemical vapour deposition (CVD) at 1100°C; (d) the epitaxial layer is lifted off – the high porosity layer serves as the breaking point; (e) the epitaxial solar cell can be finished; (f) the substrate wafer can be reused for the next PSI cycle.



However, the highest solar cell conversion efficiency achieved using the latest kerf-less technologies is only 15% [14], whereas a 19.1% conversion efficiency has been obtained by applying the PSI process [15]. To examine the entire thickness range between  $45\mu m$  and  $290\mu m$ , thinned float-zone silicon samples are also used.

#### Fabrication of BJBC solar cells

Float-zone material thinned by wet-chemical etching was used, as well as monocrystalline thin films fabricated by PSI. In this process a porous double layer is etched electrochemically into the surface of a thick silicon wafer, as shown in Fig. 1. After sintering at  $1100^{\circ}$ C in a hydrogen atmosphere, silicon is grown epitaxially on top of the closed surface of the top porous silicon layer. The growth process controls the layer thickness as well as the doping gradients. Finally, the highly porous bottom layer permits a lifting-off of the epitaxial silicon layer, and a solar cell is then processed from the thin layer. The thick silicon substrate wafer can be reused for many more PSI cycles [16,17]. The material consumption is much lower, since only the porous layer of  $2\mu$ m is lost in comparison to sawing losses of  $120\mu$ m.

The cell-thickness dependence of the efficiency will be illustrated by means of BJBC solar cells fabricated with a cell size of 3.92cm<sup>2</sup>; all the cells are processed in a single batch for better comparison of the results. A cell process previously developed at ISFH [18] is employed, which uses industrially feasible laser processes and avoids laboratory processes such as photolithography.



Figure 3. Loss analysis procedure. A simulated generation profile and the saturation current densities determined for test samples are input parameters for the finite-element simulation. Output parameters such as Fermi levels and currents are used for the free-energy loss analysis.

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| Group  | 130-1.5 | 290                           | 290-1.5   |      | 290-0.5 |      | 90-0.5                           |       | 45-0.5 |  |
|--|---------|-------------------------------|-----------|------|---------|------|----------------------------------|-------|--------|--|
| Cell thickness $d$ [µm]  | 130     | 29                            | 290       |      | 290     |      | 90                               |       | 45     |  |
| Base resistivity $ ho$ [ $\Omega$ cm]                                | 1.5     | 1.                            | 1.5       |      | 0.5     |      | 0.5                              |       | 0.5    |  |
| Base lifetime $\tau$ [µs]  | 4000    | 40                            | 4000      |      | 3000    |      | 3000                             |       | 20     |  |
| Number of processed cells  | 1       | ſ                             | 6         |      | 8       |      | 12                               |       | 3      |  |
|  | best    | best                          | 6 best    | best | 6 best  | best | 6 best                           | best  | 3 best |  |
| Open circuit voltage $V_{\rm oc}$ [mV]                               | 671     | 672                           | 672       | 673  | 673     | 672  | 669                              | 651*  | 653    |  |
| Short circuit current density J <sub>sc</sub> [mA·cm <sup>-2</sup> ] | 41.1    | 40.9                          | 40.6      | 39.7 | 39.2    | 38.4 | 37.5                             | 36.0* | 35.3   |  |
| Fill factor FF [%]   | 81.8    | 81.9                          | 80.2      | 81.6 | 81.3    | 81.9 | 80.2                             | 80.6* | 79.8   |  |
| Conversion efficiency $\eta$ [%]                                     | 22.6    | 22.5                          | 21.9      | 21.8 | 21.4    | 21.1 | 20.1                             | 18.9* | 18.4   |  |
| $\Delta\eta$ caused by difference in:                                |         | _ cell thickness              | thickness |      | cell th |      | nickness                         |       |        |  |
| $\Delta\eta$ caused by difference in:                                |         | base resistivity and lifetime |           |      |         |      | base lifetime and cell thickness |       |        |  |
| *independently confirmed by Fraunhofer ISE                           |         |                               |           |      |         |      |                                  |       |        |  |

Table 1. Material properties and parameters of the light *J*-*V* curves of the five groups investigated in this study. The best cell is shown, as are the average values of the six best cells and of the three best cells.

The cell structure is shown in Fig. 2. The front surface is textured and a 10nm-thick AlO<sub>x</sub> passivation layer is deposited by atomic layer deposition. A SiN<sub>x</sub> laver serves as an anti-reflection coating. The rear side is processed as an interdigitated finger structure with an index of 1mm. The phosphorous emitter with a sheet resistance of  $70\Omega/$ sq covers 84% of the cell rear side. A boron-diffused back-surface field (BSF) with a sheet resistance of  $20\Omega/sq$ reduces the recombination rate beneath the contacts. A thermal oxide of thickness 150nm serves as a rear-side passivation and rear reflector. Laser contact opening (LCO) of the passivation layer and subsequent aluminium evaporation form the contacts. This 10µm-thick aluminium layer is etched at the edges separating the emitter and the BSF layer [20].

Five different groups of cells – categorized according to cell thickness and base resistivity – were investigated. Table 1 shows the material properties and parameters of the light *J*-*V* curves of the processed groups. Cell thicknesses varied from 45 $\mu$ m to 290 $\mu$ m, base resistivities from 1.5 $\Omega$ cm to 0.5 $\Omega$ cm and base lifetimes from 20 $\mu$ s to 4000 $\mu$ s.

#### Loss analysis of BJBC solar cells by means of device simulations

The loss mechanisms in the experimental devices are analyzed by determining the generation, recombination and transport losses. The generation is simulated using





the ray tracer SUNRAYS [21]. Input parameters are measured geometries and optical layer properties. To determine the recombination at the surfaces, the Kane-Swanson method [22] is used, which is based on infrared lifetime measurements [23] on test samples that are processed in parallel to the solar cells. The saturation current densities of all passivated and metalized surfaces [24] are determined. The base lifetime is extracted by varying the thickness of these test samples [25].

As shown in Fig. 3 the generation profile from the SUNRAYS simulation (Fig. 3(a)) and the recombination parameters (Fig. 3(b)) are input parameters for a transport simulation (Fig. 3(c)). The transport simulation uses the conductive boundary (CoBo) model [26], which is implemented in the finite-element analyzer COMSOL [27]. The CoBo model treats diffused surfaces as one-dimensional boundaries characterized by a sheet resistance and a saturation current density. A free-energy loss analysis [28] based on the finiteelement simulation yields the generated free-energy power densities lost by different mechanisms and extracted as shown in Fig. 3(d).

Fig. 4 shows the simulated power densities at the maximum power point of the five experimentally investigated groups, which are irradiated with an intensity of 1000Wm<sup>-2</sup>: the generated and both the simulated and measured extracted power densities are plotted. The main power density losses and the sum of all losses are also shown. The extracted power densities of the simulations are about 10Wm<sup>-2</sup> (corresponding to 1% efficiency points) higher than the measured values. This deviation is attributed to resistive losses at the contacts and in the metal grids (these losses are not implemented in our simulations).

Fig. 5 shows the local minority-carrier current paths; the colour quantifies the power density loss by Shockley-Read-

Cell

Hall (SRH) recombination of the five investigated groups. The minority-carrier current paths start very close to the front surface of the unit cell, and most of them end at the rear surface of the cell. The electrons which follow the paths to the emitter and are not lost by recombination are collected and contribute to the power output. The electrons which follow the other paths are all lost by recombination. The effect of the current paths ending at the rear surface of the base finger is called electrical shading [29]: this area is indicated by a black line on top of the cells.

The simulated impact of cell thickness, base doping and base lifetime on the conversion efficiency and on the local recombination and minority carrier current paths will be discussed next.

## Impact of cell thickness on conversion efficiency

The thickness dependence is best analyzed by comparing the results of groups 290-0.5 and 90-0.5 or 290-1.5 and 130-1.5, which differ in thickness only, as shown in Table 1. At long wavelengths, the spectral response of thin cells is not as good as thick cells: the generated power density therefore decreases with decreasing cell thickness by 5% relative at a base resistivity of  $1.5\Omega$ cm and by 10% relative at a base resistivity of  $0.5\Omega$ cm.

The free-energy transport loss of electrons is the highest power density loss for all thickness values, but shows a strong decrease with decreasing cell thickness. The free-energy transport loss of electrons is a quadratic function of the electron quasi-Fermi level gradient. Since this gradient decreases with increasing distance to the emitter, the total electron transport loss  $F_{bt_e}$  increases with an exponent *x* of less than one with increasing distance to the emitter and thus with increasing cell thickness *d* ( $F_{bt_e} \sim d^x, x < 1$ ).

All power density losses caused by recombination in the base (SRH recombination, Auger recombination) or at the front surface decrease with decreasing cell thickness. The SRH recombination increases with increasing distance to the emitter because of an increase in minority carrier concentration, illustrated by comparing Figs. 5(a) and 5(c) with Figs. 5(b) and 5(d) respectively. The bottom part of cell 290-0.5 shows nearly the same local SRH recombination as cell 90-0.5; a comparison of cell groups 290-1.5 and 130-1.5 indicates the same effect. This characteristic is due to the guasi-Fermi level gradient of the minorities that causes an increase in minority-carrier concentration with increasing distance to the emitter.

On the other hand, the power density losses caused by the rear surface (emitter recombination, BSF recombination and base contact recombination) increase only



Figure 5. SRH recombination and minority-carrier current paths (black lines) of each unit cell. For comparison purposes the first four cells (a) to (d) are plotted on the same scale, whereas cell 45-0.5 has the highest SRH recombination and therefore uses a wider range. The regions of the contacts, emitter and electrical shading are shown for each cell. (Adapted from Haase et al. [19].)

slightly with decreasing cell thickness. The number of minority-carrier current paths which end in the base contact, where the electrons recombine, slightly increases with decreasing cell thickness. For these two reasons a low recombination at the base finger, and especially at the base contact, becomes more important for thinner cells.

"Thinner cells benefit from lower front and base recombination, but at the same time suffer from a reduced generation."

In conclusion, thinner cells benefit from lower front and base recombination, but at the same time suffer from a reduced generation. Depending on the specific material properties, a decrease in cell thickness might thus result in either a decrease or an increase in cell efficiency. In the study presented here, decreasing the cell thickness from 290 $\mu$ m to 130 $\mu$ m for 1.5 $\Omega$ cm and 4000 $\mu$ s material leads to a decrease in conversion efficiency of 0.5% absolute. However, decreasing the cell thickness from 290 $\mu$ m to 90 $\mu$ m for 0.5 $\Omega$ cm and 3000 $\mu$ s material leads to a decrease in conversion efficiency of only 0.2% absolute.

## Impact of base-doping on conversion efficiency

The base-doping dependence is analyzed by comparing the results of groups 290-1.5 and 290-0.5, which differ only in base doping, as shown in Table 1. The base lifetime of both samples does not differ significantly. The power densities are free energies and proportional to the quasi-Fermi level splitting. Decreasing the base resistivity and thus increasing the basedoping density lowers the Fermi level in *p*-type cells. This leads to an increase in quasi-Fermi level splitting, resulting in an increase in generated power density as well as in power density losses.

The transport loss of electrons is the highest power density loss for both doping densities and increases with increasing base doping. Since the quasi-Fermi level splitting in the base increases but is on the same level at the emitter, the gradient of the electron quasi-Fermi level increases with increasing base doping, which increases the free-energy loss by electron transport.

Auger recombination is proportional to  $(n \times p^2)$  at low-level injection in these *p*-type solar cells. For this reason, Auger recombination increases by a factor of about nine when base doping *p* increases by a factor of three, which is the case for a decrease in base resistivity from 1.5 $\Omega$ cm to 0.5 $\Omega$ cm.

Figs. 5(a) and 5(c) show that the loss by SRH recombination in cell 290-1.5 is 17% lower than in cell 290-0.5. The reason for this is a higher diffusion length and a lower quasi-Fermi level splitting in 290-1.5. Both cell groups, however, are not limited by this loss mechanism. The emitter recombination is the only loss mechanism which decreases with decreasing base resistivity. The electrical shading affects a larger part of the cell at a lower base resistivity (0.5 $\Omega$ cm) than at a higher base resistivity (1.5 $\Omega$ cm), as illustrated in Fig. 5.

All these effects lead to the conclusion

that a base resistivity of  $1.5\Omega$ cm should be used instead of  $0.5\Omega$ cm, since the former results in decreased power losses by Auger, SRH and rear-surface recombination for a thickness of 290µm and a high base lifetime of 3000µs to 4000µs.

 "A base resistivity of 1.5Ωcm should be used instead of
 0.5Ωcm, since the former results in decreased power losses by Auger, SRH and rear-surface recombination."

#### Simulating the optimum conversion efficiency dependent on cell thickness, base doping and base lifetime

In order to evaluate a larger parameter space, a simulation study was carried out to analyze the impact on the solar cell conversion efficiency of base doping combined with cell thickness for different base lifetimes. The simulations are based on the same measured geometries and recombination parameters as those obtained for the experimental cells. Figs. 6 and 7 are valid for different base lifetimes of 20µs (measured on the epitaxial layer cell) and 3000µs (measured on the floatzone wafer cell). Both Figures show the solar cell conversion efficiency for doping densities of 1014 cm-3 to 1017 cm-3 and cell thicknesses of 18µm to 290µm. The arrows



Figure 6. Solar cell conversion efficiency as a function of the base doping and cell thickness for a base lifetime of 20µs. The impact of the free energy of generation as well as loss mechanisms is indicated by arrows. (Adapted from Haase et al. [19].)

indicate how the different loss mechanisms influence the conversion efficiency.

Fig. 6 shows the efficiency for a minority-carrier lifetime of 20µs. The efficiency decreases with decreasing cell thickness (lower generated free energy) and decreasing base doping. Resistive losses by majority carriers in the lateral direction also increase with decreasing cell thickness owing to an increased sheet resistance in the base. The sheet resistance

thickness and base doping. The minoritycarrier concentration increases with increasing cell thickness. This increase in carrier concentration increases SRH recombination, which decreases the efficiency. Auger recombination also increases with increasing cell thickness because of the quasi-Fermi level gradient to the front surface, which also decreases the efficiency. Auger recombination also increases quadratically with increasing base doping. For a base lifetime of 20µs, these are the main effects that lead to a maximum efficiency at a cell thickness of 45µm and a base-doping density between 1016 cm-3 and 1017 cm-3.

also increases with decreasing base-doping

concentration, which in turn decreases the

On the other hand, the transport of

electrons increases with increasing cell

conversion efficiency.

Fig. 7 shows the efficiency for a minority carrier lifetime of 3000µs. For this lifetime the effect of SRH recombination is reduced compared to the 20µs lifetime, and the diffusion length does not significantly limit efficiency in the case of cell thicknesses up to 290µm. The efficiency presents a maximum for a base-doping concentration of about 10<sup>16</sup> cm<sup>-3</sup>. The limiting parameters for thin cells with a lifetime of 3000µs are the decreased generation and the base resistance losses. The maximum efficiency is greater than 23% for cell thicknesses above 290µm, but if the thickness is reduced from 290µm to about 90µm, the power loss is less than 0.6% absolute. The generation may be enhanced by improved light trapping, whereas the base resistance losses may be reduced by a highly doped







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layer (e.g. at the front surface), which deceases the base sheet resistance but does not significantly increase the recombination. Another possibility for reducing the resistance losses is to shorten the current path lengths by changing the geometry of the cell (e.g. smaller unit cells).

Fig. 8 shows the difference between solar cell conversion efficiencies for base lifetimes of 3000 $\mu$ s and 20 $\mu$ s. The difference in conversion efficiency is less than 1% absolute at doping densities of more than 10<sup>16</sup>cm<sup>-3</sup> and cell thicknesses of less than 45 $\mu$ m. At lower doping densities and higher cell thicknesses, the difference in efficiency increases to more than 14% absolute, which is mainly due to the increase in SRH recombination.

"The highest efficiency of 22.6% was measured on a 130μm-thick, 1.5Ωcmresistivity cell with a base lifetime of 4000μs."

#### Conclusion

The fabrication and analysis of high-efficiency BJBC cells has been demonstrated. The highest efficiency of 22.6% was measured on a 130 $\mu$ m-thick, 1.5 $\Omega$ cm-resistivity cell with a base lifetime of 4000 $\mu$ s. A 290 $\mu$ m-thick cell with a resistivity of 1.5 $\Omega$ cm showed almost the same efficiency (22.5%), since an increase in generation offsets any increase in front and base recombination. The simulation study, which is based on measured input

parameters, showed the impact of the loss mechanisms on the conversion efficiency. The maximum efficiency shifts to a larger cell thickness, with increasing base lifetime for a BJBC cell. The maximum efficiency for a BJBC is around 1016 cm-3 base-doping density, since Auger recombination and transport losses by electrons increase with higher base-doping density, and lateral transport losses by holes increase with lower base-doping density. BJBC cells with cell thicknesses of about 45µm allow a reduced material consumption combined with a high conversion efficiency of about 21%, assuming a base lifetime of 3000µs, which is only reduced by about 1% absolute if the base lifetime is reduced to 20µs. BJBC cells with base lifetimes of 3000µs show an efficiency of more than 23% for cell thicknesses greater than 290µm; this is only reduced by 0.6% absolute if the cell thickness is reduced from 290µm to 90µm.

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